

14 September 2013

Chapter 3: Evolution of the 2-body orbit

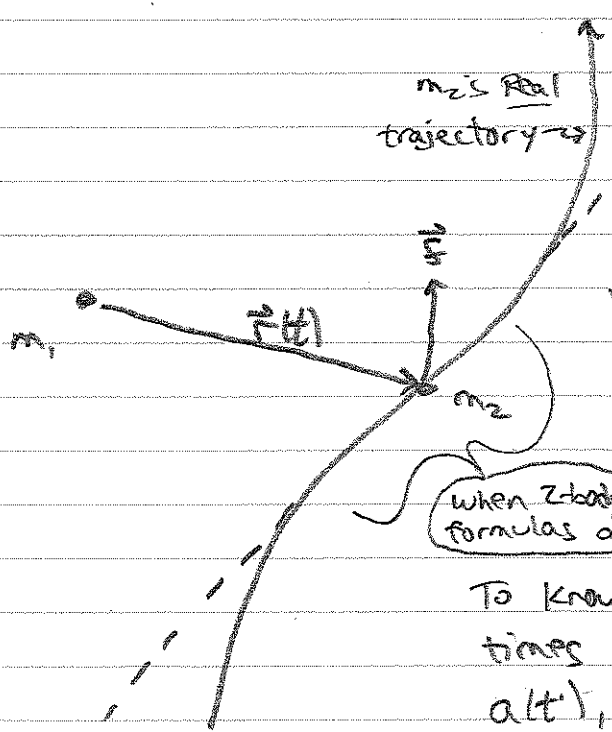
In the 2-body problem, the secondary's motion about primary m_1 is described by six constant orbit elements: $a, e, i, \omega, \Omega, \tau$

But if m_2 is perturbed by other forces, gravity from another planet, or a drag force, then the orbit elements vary with time t .

So $a(t), e(t), etc$ are NOT constants

these are m_2 's osculating orbit elements

↑ Latin: to kiss (ie, m_2 's osculating orbit is tangent to real orbit at time t)



← m_2 's osculating orbit

suppose m_2 is perturbed by force \vec{F} , and m_2 's osc. elements $a(t), e(t), i(t)$ are known at time t .

when 2-body formulas are adequate

To know where m_2 is at different times t' , you need to know $a(t'), e(t'), i(t')$ etc

which we compute from Gauss' planetary Eqs.

However, you can still use Mars osc' $a(t), e(t)$ etc to estimate where at nearby times $t + \Delta t$

using 2-body formula (eg, solve Kepler's eqn for E_c at time $t + \Delta t$ then use $r(t + \Delta t) = a(1 - e \cos E_c)$ to get $\vec{r}(t + \Delta t)$)

which is adequate provided Δt is sufficiently small.

For example, one often uses 2-body formula + osculating elements to estimate where an asteroid will be a few years hence.

But asteroids are subject to weak perturbing forces [resonances with Jupiter and Mars + Yarkovsky effect (force due to asymmetric re-radiation of incident sunlight)] which might cause large changes in a, e etc over large periods of time ($\sim 10^3$ or 10^6 yrs?)

So if you are an astronomer that wants to observe this asteroid 6 months from now, use osculating orbit elements to easily calculate $\vec{r}(t + 6 \text{ months})$, which will tell you where to point your telescope.

but if you are a planetary dynamicist, and you want to know if the YE is going to cause that asteroid to drift into resonance w/ Jup say 10⁵ yrs from now (which is how most asteroids get ejected from asteroid belt), then you would use Gauss Eqn's to estimate the orbit drift time.

Should I add YE to syllabus?

same Gauss of Gauss' Law.

Gauss' Planetary Eqn's (PE)

secondary m_2 orbits primary m_1 , and m_2 is subject to perturbing acceleration

$$\vec{a}_p = a_r \hat{r} + a_\theta \hat{\theta} + a_n \hat{n}$$

in cylindrical coordinates, where \hat{n} is normal to m_2 's orbit

so we are using orbit-plane coordinate system.

perturbation \vec{a}_p causes m_2 's a, e, i etc to vary over time

derive rates $\dot{a} = \frac{da}{dt}$, \dot{e} , $\frac{di}{dt}$ etc
= Gauss' PE

calculate \dot{q}

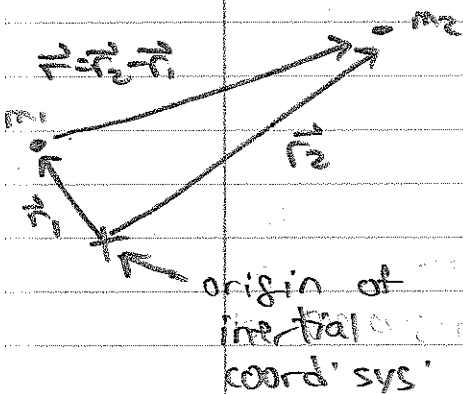
$$W = m_2 \int_{\vec{r}_1}^{\vec{r}_2} \vec{a}_p \cdot d\vec{r} = \text{work done on } m_2 \text{ by acceleration } \vec{a}_p$$

so $\Delta W = m_2 \vec{a}_p \cdot \Delta \vec{r} = \text{small work done on } m_2 \text{ during small displacement } \Delta \vec{r}$

$$\dot{W} = \frac{\Delta W}{\Delta t} = m_2 \vec{a}_p \cdot \dot{\vec{r}}_2$$

= rate at which work is done on m_2

= rate at which m_2 's energy changes in inertial coordinate system



you will show in problem 2.4 shows

$$\dot{\vec{r}}_2 = \frac{\mu_r}{m_2} \dot{\vec{r}}$$

where $\mu_r = \frac{m_1 m_2}{m_1 + m_2} = \text{reduced mass}$

so $\dot{W} = \mu_r \vec{a}_p \cdot \dot{\vec{r}} = \text{rate } m_2 \text{'s energy } E \text{ changes}$

= rate at which system total energy E changes

Prob 2.4: the system's total energy

$$E = \mu r \dot{\epsilon} \quad \text{where } \dot{\epsilon} = -\frac{\mu}{2a}$$

$$= 2\text{body energy integral}$$

$$\text{so } \dot{W} = \mu r \vec{a}_p \cdot \dot{\vec{r}} = \mu r \dot{\epsilon} = \frac{\mu r \mu a}{2a^2}$$

$$\text{so } \dot{a} = \frac{2a^2 \vec{a}_p \cdot \dot{\vec{r}}}{\mu} = \frac{2\vec{a}_p \cdot \dot{\vec{r}}}{\mu^2 a}$$

$$= \frac{2}{\mu^2 a} \left(a_r \dot{r} + a_\theta r \dot{\theta} + a_n \dot{z} \right)$$

what is m_2 's \dot{z} measured in the orbit-plane coordinate system?

recall $\dot{r} = \frac{ea_n \sin f}{\sqrt{1-e^2}}$ $r\dot{\theta} = r\dot{f} = \frac{an}{\sqrt{1-e^2}} (1+e\cos f)$

$$\text{so } \dot{a} = \frac{2}{\mu^2 a} \left[a_r e \sin f + a_\theta (1+e\cos f) \right]$$

usually one uses Gauss' Eqns when doing analytic work, which usually requires $e \ll 1$, so for nearly circular orbits

$$\dot{a} \approx \frac{2a\dot{a}}{n} \quad \left(\begin{array}{l} \text{for example, orbit decay} \\ \text{due to drag has } \dot{e} \approx 0 \\ \text{so } e \text{ usually small} \end{array} \right)$$

⇒ the tangential or 'along-track' part of the perturbing acceleration \vec{q}_p will cause semi-major axis a to grow or shrink.

to get di/dt :

set $\vec{h} = h\hat{n} = m_2$'s angular momentum
integral

so $\vec{\tau} = \frac{d\vec{h}}{dt} =$ specific torque on m_2

use right-hand fingers to evaluate cross products, A.18

$$= \vec{\tau} \times \vec{q}_p = r\hat{r} \times (a_r\hat{r} + a_\theta\hat{\theta} + a_n\hat{n}) \quad \leftarrow$$

$$= r a_\theta \hat{n} - r a_n \hat{\theta}$$

$$= \dot{h}\hat{n} + h \frac{d\hat{n}}{dt}$$

$$\text{so } \dot{h} = r a_\theta$$

$$\text{and } \frac{d\hat{n}}{dt} = -\frac{r a_n}{h} \hat{\theta} = \frac{r a_n}{h} \hat{r} \times \hat{n}$$

so a_θ alters the magnitude of \vec{h} ,
 and a_n alters the direction \vec{h} points towards
 ie only normal acceleration a_n
 can tip m_2 's orbit plane

since $h = \sqrt{\mu a (1-e^2)}$

$$\dot{h} = \frac{1}{2} \sqrt{\frac{\mu(1-e^2)}{a}} \dot{a} + \frac{1}{2} \sqrt{\frac{\mu a}{1-e^2}} (-2e\dot{e}) = -ra_\theta$$

so $\dot{e} = \frac{1}{e} \sqrt{\frac{1-e^2}{\mu a}} \left(\frac{1}{2} \sqrt{\frac{\mu(1-e^2)}{\mu a}} \dot{a} - ra_\theta \right)$

$\mu = n^2 a^3$

$$\dot{e} = \frac{\sqrt{1-e^2}}{ea^2 n} \left\{ \frac{an}{2} \frac{\sqrt{1-e^2}}{n\sqrt{1-e^2}} \left[a e \sin f + a_\theta (1 + e \cos f) \right] - ra_\theta \right\}$$

$$\text{so } \dot{e} = \frac{\sqrt{1-e^2}}{ean} \left[a e \sin f + a_\theta \left(1 + e \cos f - \frac{r}{a} \right) \right]$$

if we use $r = a(1 - e \cos E)$

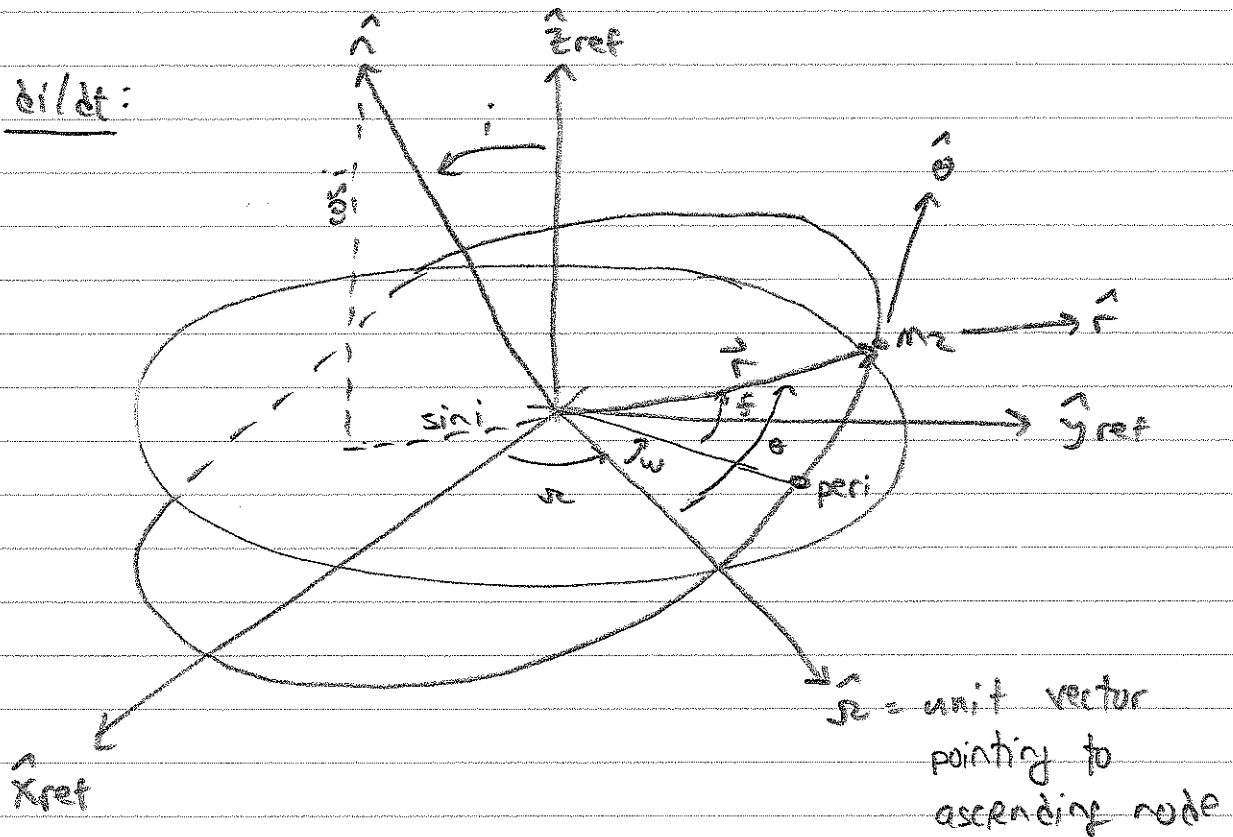
then the e in the denominator goes away

for $e < 1$ since $f = E + \theta(t)$ P.

$$\dot{e} = \frac{1}{an} (ar \sin f + 2a_0 \cos f)$$

$$\dot{e} = \frac{\sqrt{1-e^2}}{an} \left[ar \sin f + a_0 (\cos f + \cos f) \right]$$

\dot{e}/dt :



$$\dot{\hat{z}}_{ref} = \dot{\hat{n}} = \cos i$$

$$\begin{aligned} \text{so } \frac{d}{dt} \hat{z}_{ref} \cdot \hat{n} &= \hat{z}_{ref} \cdot \frac{d\hat{n}}{dt} = -\sin i \frac{di}{dt} \\ &= \frac{r a n}{h} \hat{z}_{ref} \cdot (\hat{n} \times \dot{\hat{n}}) \end{aligned}$$

now use vector identity A.B:

$$\vec{a} \cdot (\vec{b} \times \vec{c}) = \vec{b} \cdot (\vec{c} \times \vec{a}) = \vec{c} \cdot (\vec{a} \times \vec{b})$$

$$\text{so } \frac{di}{dt} = -\frac{r a_n}{h \sin i} \hat{r} = (\hat{n} \times \hat{z}_{\text{ref}})$$

what is this?
use right fingers

$$\hat{n} \times \hat{z}_{\text{ref}} = -\sin i \hat{\Omega}$$

$$\text{also note } \hat{r} \cdot \hat{\Omega} = \cos(\omega + f)$$

$$\text{so } \frac{di}{dt} = -\frac{r a_n}{h \sin i} (-\sin i) \cos(\omega + f)$$

$$\frac{di}{dt} = -\frac{r a_n}{h} \underbrace{\cos(\omega + f)}_{\theta}$$

for nearly circular orbits, $h = r^2 \dot{\theta} \approx a^2 n$

$$\text{and } \frac{di}{dt} \approx \frac{a_n}{a n} \cos \theta$$

only normal accelerations a_n drive i -evolution

step
Sept 17

calculate $\dot{\mathcal{R}}$ = rate at which $\hat{\mathcal{R}}$ moves

let $\vec{\Delta n}$ = change in \hat{n} during time Δt
due to perturbation \vec{a}_p

$$\vec{\Delta n} = \text{sum of 3 orthogonal parts} \\ = a\hat{n} + b\hat{\mathcal{R}} + c(\hat{n} \times \hat{\mathcal{R}})$$

where a, b, c are coefficients to be determined:

$$a = \vec{\Delta n} \cdot \hat{n} \quad \rightarrow \text{change in } \hat{n} \text{ along } \hat{n}$$

$$b = \vec{\Delta n} \cdot \hat{\mathcal{R}}$$

$$c = \vec{\Delta n} \cdot (\hat{n} \times \hat{\mathcal{R}}) \quad \rightarrow \text{corresponds to rotating} \\ \text{orbit plane about } \hat{\mathcal{R}} \text{ axis}$$

Does moving \hat{n} along the \hat{n} or $\hat{n} \times \hat{\mathcal{R}}$
axes change \mathcal{R} ?

If not, then we can ignore the
 a, c components, and focus on the

$\vec{\Delta n} \cdot \hat{\mathcal{R}}$ component that causes
 \mathcal{R} to increment by $\Delta \mathcal{R}$ in time Δt

The derivations of the rates for the remaining elements, $\dot{\omega}$ and $\dot{\Omega}$, are laborious.

But they are easy to obtain when $e \ll 1$ and the orbit is nearly circular, which is the regime where we will use these eqn's anyway

To get $\dot{\omega}$,
Start with $r = a(1 - e \cos E)$

$$\approx a(1 - e \cos f) + \mathcal{O}(e^2)$$

$$\text{so } \dot{r} \approx \dot{a}(1 - e \cos f) - a e \sin f \dot{f} + e a \dot{f} \sin f$$

$$\approx \frac{e a n \sin f}{\sqrt{1 - e^2}} \quad (\text{from 2-body problem})$$

$$\approx e a n \sin f$$

The true anomaly $f = \theta - \tilde{\omega}$ ← long of asc. node

$$\text{so } \dot{f} = \dot{\theta} - \dot{\tilde{\omega}} \quad \text{where } \dot{\theta} \approx n + \mathcal{O}(en)$$

$$\approx n - \dot{\tilde{\omega}} + \mathcal{O}(en)$$

$$\text{insert this } + \dot{a} \approx \frac{2a\dot{a}}{n} \quad \text{and} \quad \dot{e} \approx \frac{a}{an} \dot{a} \sin f + \frac{2a\dot{a}}{an} \cos f$$

$$\frac{2a\dot{a}}{n} (1 - \mathcal{O}(e)) - \frac{a \cos f}{an} (a n \sin f + 2a\dot{a} \cos f) + e a (n - \dot{\tilde{\omega}}) \sin f$$

$$\approx e a n \sin f$$

$$\text{so } \frac{2ab}{n} - \frac{ar}{n} \sin f \cos f - \frac{2a^2}{n} \cos^2 f = ea \hat{\omega} \sin f$$

$(-\sin^2 f)$
 \downarrow

$$-\frac{ar}{n} \sin f \cos f + \frac{2a^2}{n} \sin^2 f = ea \hat{\omega} \sin f$$

$$\text{so } \hat{\omega} = \frac{2ab \sin f - ar \cos f}{ean} \quad \text{to lowest order in } e$$

To get \hat{t} ,

start with $M = n(t - \tau) = \text{mean anomaly}$

$$= f + \theta(e) \quad \text{since } f = M + 2e \sin M$$

$$\text{so } \hat{M} = f = n \hat{\omega} = \hat{n}(t - \tau) + n(1 - \hat{t})$$

$$= \hat{n}M/n + n - n\hat{t}$$

$$\text{Note } \hat{n} = \sqrt{\mu} a^{-3/2} \quad \text{so } \dot{\hat{n}} = -\frac{3}{2} \frac{n}{a} \dot{a} = \frac{-3ab}{a}$$

$$\text{and } n\hat{t} = -\frac{3ab}{an} M + n - n + \hat{\omega}$$

$$\text{so } \hat{t} = \frac{2ab \sin f - ar \cos f}{ean^2} - \frac{3ab}{an} (t - \tau)$$

These formula for $\hat{\omega}$ and \hat{t} are only valid when e and i are $\ll 1$. See reference [1] by Burns (1976) for exact derivation of $\hat{\omega}, \hat{t}$

Let's examine orbital decay of interplanetary dust, due incident sunlight... aka PR drag

The solar system is full of dust of radii $10^2 \lesssim R \lesssim 10^3 \mu\text{m}$,
 comets come close to sun, $r \lesssim 1.5 \text{ AU}$,
 their icy surfaces sublimate (boil off),
 flowing gas drags dust away, producing
 cometary comae and tails (see text fig 34)
 all that comet dust goes into orbit about sun.

Asteroids also collide and produce dust,
 first-eye collision detected by Hubble in 2010
 (look up P/2010 A2)

The resulting cloud of dust orbits the sun,
 you can see it right after sunset or
 just before sunrise - the zodiacal light.

These grains orbit the sun,
 but the absorption & re-radiation of sunlight
 results in a drag force on the grain -
 Poynting-Robertson (PR) drag,
 which causes dust to slowly spiral into sun.

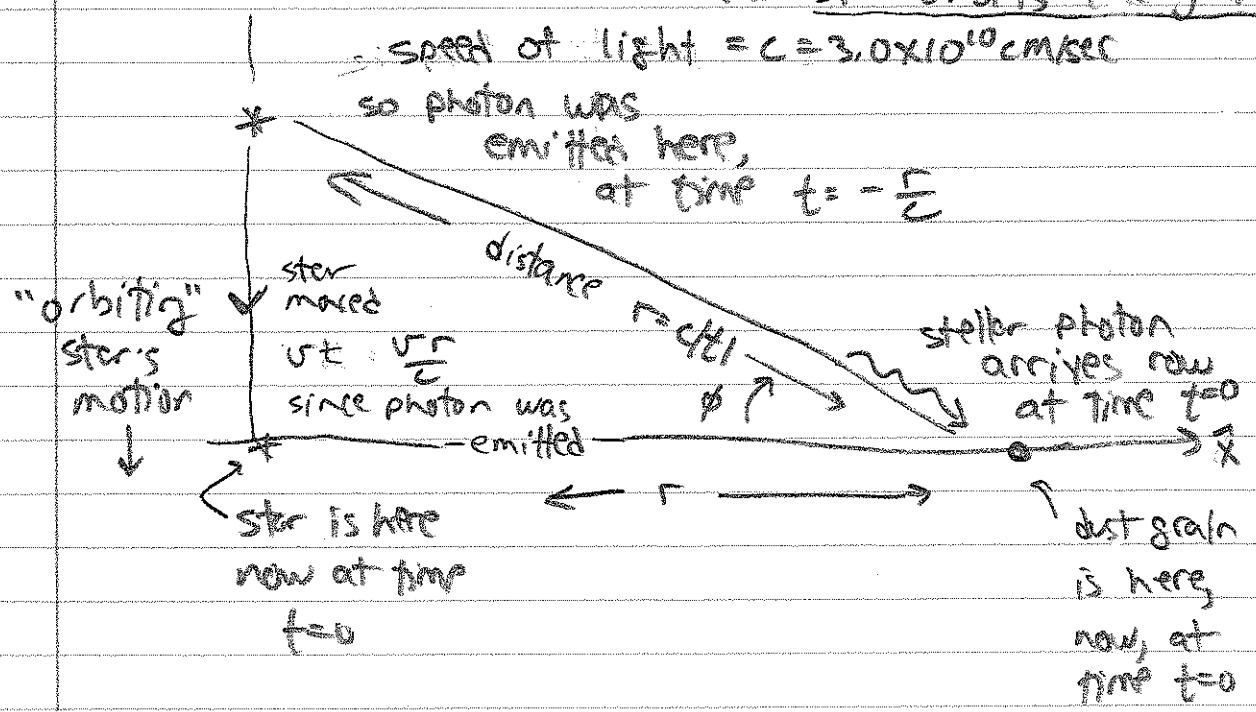
orbit decay due to PR drag

PR drag is analogous to driving in the rain, the faster you drive, the harder the rain seems to pelt the front windshield, less so in the rear.

Ditto for a dust grain travelling thru a storm of photons:

PR drag is due to stellar aberration: the apparent displacement of a star due to an observer's motion (usually an astronomer on an orbiting Earth)

Let's put our coordinate system on the orbiting dust grain. In this coordinate system the star orbits the grain



Suppose you are riding on the grain,
and you look back along the photon's path
to you - you see a star, but it isn't
really located where you are looking

The finite speed of light causes the star
to appear to be displaced by angle $\varphi = \frac{v}{c}$
(stellar aberration)

Note: to solve this problem exactly, one must
use relativistic Lorentz transformations,
which we will not do. But when dust
grain's orbital speed obeys $v/c \ll 1$,

the exact solution reduces to the non-relativistic
solution obtained here.

First, note that $F_0 = \frac{L_*}{4\pi r^2}$ would be

the flux (eg, rate-per-area) of photon-energy

incident upon the grain, where

$L_* = \text{star's luminosity}$ (= rate at which star emits energy)

But if the grain has radial velocity v ,
then photons of wavelength λ_0 are

Doppler shifted by

for non-relativistic
orbital speeds, $v \ll c$

$$\frac{\lambda}{\lambda_0} = 1 + \frac{v}{c}$$

recall that a photon's energy is

$$E = h\nu = \frac{hc}{\lambda}$$

Planck constant

$$\Rightarrow E \propto \lambda^{-1}$$

and L_γ and F get boosted by factor $(1 + \frac{v}{c})^{-2} \approx 1 - \frac{v}{c}$

so $F_{\text{obs}} = (1 - v/c) F_0$ is flux of Doppler-shifted photons hitting the dust grain

These photons deliver energy to grain

at rate $\dot{E} = F_{\text{obs}} A$ where $A = \text{grain's cross-sectional area} = \pi R^2$

photons carry momentum $p = E/c$

so starlight delivers momentum to grain at rate $\dot{p}_{\text{inc}} = \dot{E}/c$

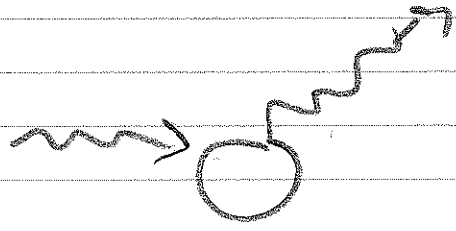
$$= \frac{1}{c} (1 - \frac{v}{c}) F_0 A$$

A dust grain can do 3 things w/ incident photon:

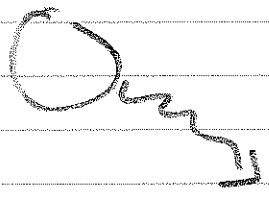
1. it can absorb the photon (which heats) grain up



2. dust can scatter photon away



3. or grain can emit a new photon (e.g., radiate in IR), which cools grain



Each event alters the grain's momentum $\vec{p} = m\vec{v}$. So Newton's 2nd law for the grain is

$$m\ddot{\vec{r}} = \dot{\vec{p}}_{\text{abs}} + \dot{\vec{p}}_{\text{scat}} + \dot{\vec{p}}_{\text{emis}}$$

← for radiative processes only, ignoring stellar gravity for now

← perturbing force

= rates at which grain's \vec{p} varies due to absorption + scattering of starlight + grain's thermal emission.

of course the dust grain is bombarded by countless photons each second, so we should replace \dot{m}_r^i with its time-average:

$$\dot{m}_r^i \rightarrow \langle \dot{P}_{abs} + \dot{P}_{scat} + \dot{P}_{emis} \rangle$$

average
= rate of grain's momentum change as it recoils from incident light

We don't know what the RHS looks like in detail, but it probably (but see exception below) has the form:

$$\langle \dot{P}_{abs} + \dots \rangle = Q_{pr} \dot{p}_{inc} \hat{p}$$

where \dot{p}_{inc} = rate at which grain's momentum would change if

$$Q_{pr} = \text{radiation pressure efficiency} = 1$$

for instance, if the dust grain absorbed all incident sunlight and scattered light isotropically in its rest frame $\langle \dot{P}_{scat} \rangle = 0$, and its thermal emission were isotropic, $\langle \dot{P}_{emis} \rangle = 0$, then $Q_{pr} = 1$ (for perfectly absorbing grain)

But what if the grain was instead a perfect reflector of sunlight?

$$Q_{pr} = ?$$

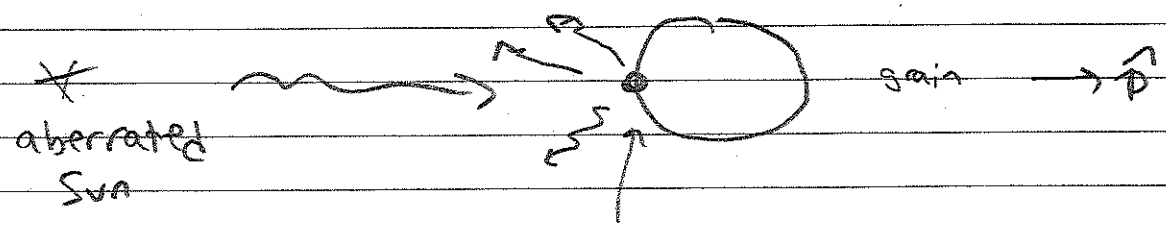
so the remainder will assume that

$$\dot{m} \vec{r} = \langle \dot{P}_{abs} \rangle + \langle \dot{P}_{scat} \rangle + \langle \dot{P}_{emiss} \rangle = Q_{pr} \dot{P}_{inc} \hat{p}$$

but this is only true under certain conditions. The concern is the

$\langle \dot{P}_{emiss} \rangle$ term, ... This is the rate

at which the grain recoils due to its thermal emission, the grain is heated by optical sunlight that is later re-radiated at IR wavelengths.

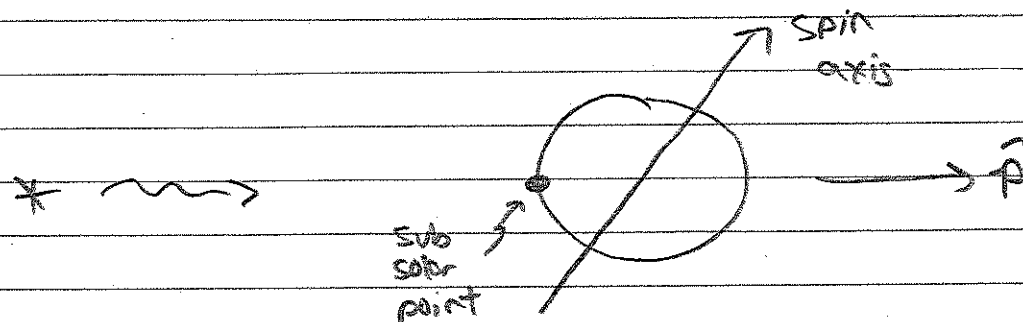


grain's sub-solar point receives most sunlight

If grain is not rotating (or rotating slowly enough), then the sub-solar point acts like a photon jet. Then $\langle \dot{P}_{emiss} \rangle \propto \hat{p}$

and the above formulas are OK.

But what if the grain is rotating?



$\langle \vec{F}_{\text{spin}} \rangle$ does NOT necessarily point anti-sunward along \vec{p}

\Rightarrow The grain's warmer side acts like a photon jet that drives additional orbit evolution that is not accounted for by the following equations; that evolution is known as the Yarkovsky effect (YE)

YE is significant: high-precision monitoring of spacecraft (LAGEOS, for example)

And asteroid orbit evolution, especially asteroids of sizes

$$0.1 \leq R \leq 1 \text{ km}$$

ex: $R \sim 100 \text{ m}$ - sized asteroids in asteroid belt slowly drift into orbital resonance w/ Jupiter, which can kick asteroid into Mars-crossing orbit

which can then kick the asteroid down to perihelion $q < 1.3 \text{ AU}$, and the asteroid is then classified as a Near Earth Object (NEO).

NEOs are now the preferred destination for NASA missions (manned & unmanned)

most NEOs likely spent billions of years in asteroid belt at $2 \lesssim a \lesssim 3 \text{ AU}$, but only recently drifted into Near-Earth space via YE.

NEOs (and comets) are also impact hazards, tho that threat is usually overblown... no-one has died from asteroid impact during all of recorded history.

...end of digression.

But a small $R \sim 100 \mu\text{m}$ dust grain likely does not suffer YE.

When a grain absorbs a photon, that causes a thermal wave to propagate across the grain. If the grain is small enough, the thermal wave can cross the grain "soon enough" to equalize the grain's surface temperature, which then makes

$$\langle \dot{T}_{\text{emiss}} \rangle = 0$$

ie, depends on grain's thermal conductivity & thermal inertia

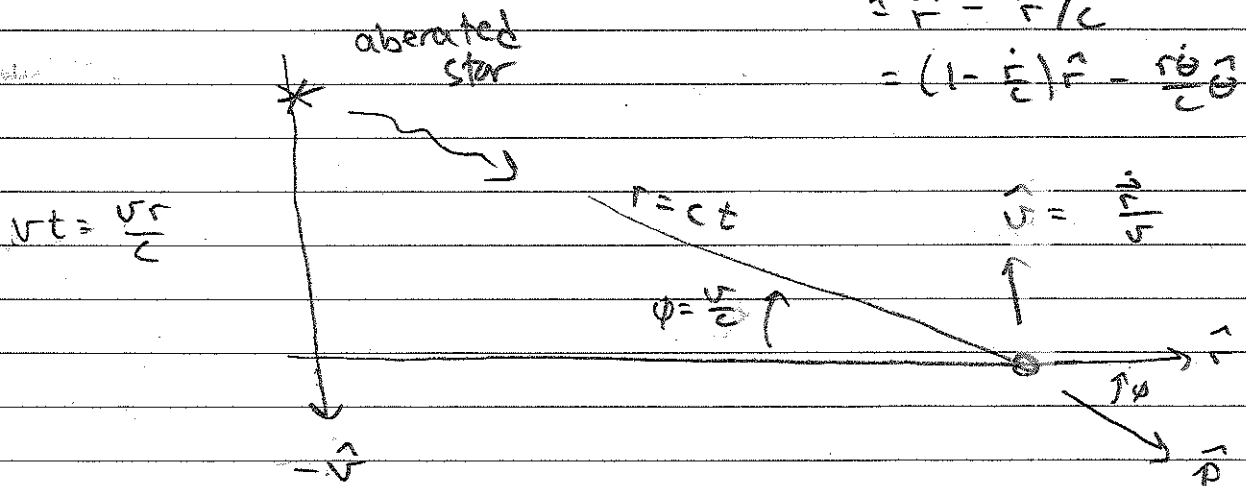
This is why $R \sim 100m$ asteroids suffer YF,
 They are too large for thermal conduction
 to equalize their surface temperatures
 so $\langle \dot{p}_{emiss} \rangle \neq 0$.

But for the dust grain,

$$m \ddot{\vec{r}} = Q_{pr} \dot{p}_{inc} \hat{p} \quad \text{where} \quad \hat{p} = \cos\phi \hat{r} - \sin\phi \hat{\theta}$$

$$\hat{p} = \hat{r} - \dot{r}/c \hat{\theta}$$

$$= (1 - \dot{r}/c) \hat{r} - \frac{r \dot{\theta}}{c} \hat{\theta}$$



$$\text{and} \quad \dot{p}_{inc} = (1 - \dot{r}/c) F_0 A / c$$

$$\text{so} \quad \ddot{\vec{r}} = \frac{Q_{pr} F_0 A}{m c} (1 - \dot{r}/c) \left[(1 - \dot{r}/c) \hat{r} - \frac{r \dot{\theta}}{c} \hat{\theta} \right]$$

small terms
 since $v \ll c$

= perturbing acceleration due to sunlight.

$$\text{so} \quad \ddot{\vec{r}} \approx \frac{F_0 A Q_{pr}}{m c} \left[\left(1 - \frac{2\dot{r}}{c}\right) \hat{r} - \frac{r \dot{\theta}}{c} \hat{\theta} \right]$$

to first order in the small quantities

$$\text{set } \vec{a} = \vec{a}_{\text{rad}} + \vec{a}_{\text{PR}}$$

↑
velocity
- independent

part = radiation
pressure

↑
velocity - dependent
part = F_{rad}/A

Robertson
drag.

$$\vec{a}_{\text{rad}} = a_{\text{rad}} \hat{r}$$

$$a_{\text{rad}} = \frac{F_0 A Q_{\text{PR}}}{mc}$$

$$\text{and } \vec{a}_{\text{PR}} = -a_{\text{rad}} \left(\frac{2\dot{r}}{c} \hat{r} + \frac{r\dot{\theta}}{c} \hat{\theta} \right)$$

radiation pressure:

set $g = -\frac{GM_*}{r^2}$ = gravity
on grain
due to
primary star

$$\text{set } \beta = \frac{a_{\text{rad}}}{|g|} = \frac{r^2}{GM_*} \left(\frac{F_0}{4\pi r^2} \right) \frac{A}{\frac{4\pi}{3} \rho R^3} Q_{\text{PR}}$$

$$= \frac{3L_* Q_{\text{PR}}}{16\pi GM_* \rho R C}$$

assuming spherical
grain of radius R
density ρ .

$$= \frac{\text{radiation pressure}}{\text{stellar gravity}}$$

$$= \text{constant, independent of } r$$

$$c = 3 \times 10^{10} \text{ cm/sec}$$

For dust orbiting the sun having

$$\rho = 3 \text{ gm/cm}^3 \quad Q_{pr} = 1$$

$$\Rightarrow \beta \sim 0.2 \left(\frac{R}{\mu\text{m}} \right)^{-1}$$

$$\text{cm}^3/\text{gm}/\text{sec}^2$$

$$G = 6.67 \times 10^{-8}$$

$$M_{\odot} = 2 \times 10^{33} \text{ gm}$$

$$L_{\odot} = 4 \times 10^{33} \text{ ergs/sec}$$

so small micron-sized dust experience significant radiation pressure.

↑
note:
astro-types
use CGS
units,

energy unit

$$1 \text{ erg} = 9 \text{ m} \cdot \text{cm}^2/\text{sec}^2 \\ = 10^{-7} \text{ joules}$$

The above is valid in the geometric optics limit, i.e. the dust grain must be significantly larger than wavelength of the incident light, i.e.

$$R \gg \lambda \quad \text{where } \lambda \sim 0.6 \mu\text{m} \\ \text{for sun light.}$$

if $R \lesssim \lambda$, you need to use light-scattering theory (i.e. Mie theory) to calculate $\beta(R)$.

But interplanetary dust have $10 \lesssim R \lesssim 100 \mu\text{m}$

so our derivation is appropriate.

So the equation of motion for a dust grain that suffers radiation pressure only is

$$\ddot{\vec{r}} = -\frac{GM_{\star}}{r^2} (1-\beta) \vec{r}$$

so this grain is in a simple Keplerian orbit, but that grain behaves as if in orbit about a star whose mass is reduced by factor $1-\beta$

Assignment #3 due?
problem 3.5

Orbit decay due to PR drag:

$$\vec{a}_{PR} = a_r \vec{r} + a_{\theta} \vec{\theta} = \text{acceleration of dust due to PR}$$

where $a_r = -\frac{2q_{rad} \dot{r}}{c}$ and $a_{\theta} = -\frac{q_{rad} r \dot{\theta}}{c}$

$q = \text{grain's SMC}$

note $a_{rad} = \beta |g| = \beta \frac{GM_{\star}}{r^2} = \frac{\beta M}{r^2} = \beta \frac{n^2 a^3}{r^2}$

The grain's radial, tangential velocities are

$$\dot{r} = \frac{e a n \sin f}{\sqrt{1-e^2}} \approx e a n \sin(M) + O(e^2)$$

where $f \approx M + O(e)$

f true anomaly
 M mean anomaly

and $M = n t$

(we can set peri-passage time $\tau = 0$)

$$\text{and } r \dot{\theta} = r \dot{f} = \frac{a n (1 + e \cos f)}{\sqrt{1-e^2}} \approx a n (1 + e \cos M)$$

$$\text{and } r \approx a (1 - e \cos M)$$

$$\begin{aligned} \text{so } a_{\dot{r}} &\approx -2\beta n^2 a \left(\frac{a}{r}\right)^2 \frac{e a n}{c} \sin M \\ &\approx -2\beta e \left(\frac{a n}{c}\right) \sin M a n^2 \end{aligned}$$

to lowest order in small quantities; ex $\frac{a n}{c}$

$$\begin{aligned} \text{and } a_{\dot{\theta}} &\approx -\beta a n^2 \left(\frac{a}{r}\right)^2 \frac{a n}{c} (1 + e \cos M) \\ &\quad \downarrow \text{by binomial thm} \\ &= -\beta \left(\frac{a n}{c}\right) (1 + 2e \cos M) (1 + e \cos M) a n^2 \end{aligned}$$

$$\text{so } a_{\dot{\theta}} \approx -\beta \left(\frac{a n}{c}\right) [1 + 3e \cos M + O(e^2)] a n^2$$

to the same precision, i.e.,

the smallest terms in a_0 are $\mathcal{O}\left(\frac{e^{2\alpha n}}{c}\right)$

When Taylor expansions to approximate the equations of motion, always be consistent when dropping small terms.

If we keep only $\mathcal{O}\left(\frac{e^{\alpha n}}{c}\right)$ terms and drop smaller $\frac{e^{2\alpha n}}{c}$ terms in a_1 ,

we must do the same when simplifying a_0

For instance, if kept only the lowest order term in a_0 i.e.

$$a_0 = -\beta \left(\frac{\alpha n}{c}\right) [1 + \mathcal{O}(e)]$$

we will probably arrive at incorrect result since our a_1 is correct to $\mathcal{O}(e)$ while our a_0 is only correct to $\mathcal{O}(e^0)$

\Rightarrow be consistent when dropping higher-order e^2 terms.

To calculate grain's orbit decay rate,
insert a_r and a_e into Gauss' planetary Eqn
for \dot{a} :

$$\dot{a} = \frac{z}{n\sqrt{1-e^2}} \left[a_r \sin f + a_e (1+e \cos f) \right]$$

which is obviously a complicated mess of sinusoids

But we aren't interested in the instantaneous
value of $\dot{a}(t)$ which might vary widely
during time t .

Instead we want the time-averaged
value of \dot{a} which is the slow &
steady rate at which PR drag damps
the grain's orbit.

To proceed, write \dot{a} to order $O(e^1)$.
i.e., keep terms proportional to e^0 & e^1
but drop the e^2 and smaller terms.
This will give us a result that is then
easily time-averaged:

$$e \sin f \approx e \sin M + O(e^2)$$

$$\text{and } (1-e^2)^{-1/2} \approx 1 + O(e^2)$$

$$\text{so } \dot{a} \approx \frac{z}{n} \left(-\frac{1}{c} \right) \left(\frac{a_n}{c} \right) a_n^2 \left[2e^2 \sin^2 M \right. \\ \left. + (1+3e \cos M)(1+e \cos M) \right]$$

what terms in $[\]$ should be
preserved and neglected, consistent
with our earlier approximations?

$$\text{so } [] \approx [1 + 4e \cos M + 2e^2 \sin^2 M + 3e^2 \cos^2 M]$$

$$= [1 + 4e \cos nt + e^2 + e^2 \cos^2 nt]$$

since $M = nt$

$$\text{so } \dot{a} = -2B \left(\frac{qa}{c} \right) [1 + 4e \cos nt + O(e^2)] \text{ an}$$

lets average \dot{a} over 1 orbit:

$$\langle \dot{a} \rangle = -2B \left(\frac{qa}{c} \right) \langle 1 + 4e \cos nt \rangle \text{ an}$$

what is the time average of

$$\langle 4e \cos nt \rangle = \frac{1}{T} \int_0^T 4e(t') \cos(nt') dt'$$

where $T =$ particle's orbit period

looks complicated since grain's eccentricity $e =$ function of time.

But if PR drag is weak, then $e(t)$ varies very little during 1 orbit, we can treat $e(t) =$ constant, so

$$\langle 4e \cos(nt) \rangle = 4e \langle \cos(nt) \rangle = ?$$

$$\text{so } \dot{a} \approx -2\beta \left(\frac{an}{c} \right) an \left[1 + \mathcal{O}(e^2) \right]$$

this means that this approximate result is correct to first-order in e , and that terms neglected by our approximations are of order e^2 or smaller.

$$\text{so } \dot{a} \approx -2\beta \left(\frac{an}{c} \right) an = \text{grains sma decay rate}$$

The orbit decay time scale is

$$\tau_a = \left| \frac{a}{\dot{a}} \right| = \frac{c/an}{2\beta n}$$

$$\text{but } T = \text{orbit period} = \frac{2\pi}{n}$$

$$\text{so } \tau_a = \frac{c/an}{4\pi\beta} T$$

For a $R=1\text{mm}$ grain, $\beta \approx 0.2$

if it orbits at $a=1\text{AU}$, $T=1\text{yr}$

$$\begin{aligned} an &= \sqrt{\frac{GM_\odot}{a}} = 30 \text{ km/sec} = 3 \times 10^4 \text{ cm/sec} \\ &= \text{Kepler speed at } 1 \text{ AU} \end{aligned}$$

since $c = 3 \times 10^{10}$ cm/sec then $\frac{c}{a\Omega} = \frac{3 \times 10^{10}}{3 \times 10^6} = 10^4$

$$\Rightarrow \tau_a = 4 \times 10^3 \text{ yrs}$$

This is roughly the time it takes a $R = 1 \mu\text{m}$ grain at $a = 1 \text{ AU}$ to spiral into the sun.

To solve for the exact orbit decay timescale we need to integrate the DE

$$\frac{da}{dt} = -2\beta \frac{a^2 n^2}{c}$$

but the above expression for $\tau_a = \left| \frac{a}{\dot{a}} \right|$

provides an easy estimate of decay time scale for PR drag.

Note that $\tau_a \propto \beta^{-1} \propto R$

so an $R = 10$ or $100 \mu\text{m}$ grain (typical of interplanetary dust) decays into sun in

$$\tau \sim 4 \times 10^4 \text{ or } 5 \text{ yrs}$$

eccentricity damping by PR drag

Gauss Planetary Eqn for e :

$$\begin{aligned} \dot{e} &= \frac{\sqrt{1-e^2}}{an} \left[a_r \sin f + a_b (\cos f + \cos E_c) \right] \\ &= -\frac{\sqrt{1-e^2}}{an} \beta \left(\frac{an}{c} \right) an^2 \left[2e \sin M \sin f \right. \\ &\quad \left. + (1 + 3e \cos M) (\cos f + \cos E_c) \right] \end{aligned}$$

tricky terms

Again, time-average over an orbit period T :

$$\langle \dot{e} \rangle = \frac{1}{T} \int_0^T \dot{e}(t) dt$$

[assuming $e(t), a(t)$
are constant during
this short time interval.

and preserve on the RHS the non-zero
time-averaged terms that are lowest-order in e :

Note that the tricky terms are NOT simply
 $\cos f + \cos E_c \approx 2 \cos M$

Assignment #3 problem 2.11

$$\text{show } \cos \epsilon_c \approx \cos M + \frac{1}{2} \epsilon (\cos 2M - 1) + \mathcal{O}(\epsilon^2)$$

$$\cos f \approx \cos M + \epsilon (\cos 2M - 1) + \mathcal{O}(\epsilon^2)$$

$$\text{so } \cos f + \cos \epsilon_c \approx 2 \cos M + \frac{3}{2} \epsilon (\cos 2M - 1)$$

i.e. the $\cos f + \cos \epsilon_c \approx 2 \cos M$ approximation

neglects a constant $-\frac{3}{2} \epsilon$ on RHS

inserting this into $\langle \epsilon \rangle$ to $\mathcal{O}(\epsilon^1)$ yields:

$$\langle \epsilon \rangle \approx -\beta \left(\frac{qA}{\epsilon} \right) \langle 2 \epsilon \sin^2 M \rangle$$

$$+ (1 + 3\epsilon \cos M) \left(2 \cos M + \frac{3}{2} \epsilon (\cos 2M - 1) - \frac{3}{2} \epsilon \right)$$

what is $\langle \sin^2 M \rangle$?

$$= \frac{1}{T} \int_0^T \sin^2(\omega t') dt'$$

$$= \frac{1}{T} \int_0^T \left(\frac{1}{2} - \frac{1}{2} \cos 2\omega t' \right) dt'$$

$$\text{so } \langle \sin^2 M \rangle = \frac{1}{2}$$

we also need

$$\begin{aligned} & \langle 2\cos\theta + \frac{3}{2}e\cos\theta - \frac{3}{2}e + b\cos^2\theta + O(e^2) \rangle \\ & = 0 + 0 - \frac{3}{2}e + 3e = \frac{3}{2}e \end{aligned}$$

$$\text{so } \langle \dot{e} \rangle = -\beta \left(\frac{a n}{z} \right) n \left(e + \frac{3}{2}e \right)$$

$$= -\frac{5}{2} \beta \left(\frac{a n}{z} \right) e n$$

= grains e-damping rate
due to PR drag

$$\begin{aligned} \text{so } \tau_e &= \left| \frac{e}{\langle \dot{e} \rangle} \right| = \frac{z(c/a n)}{5\beta n} = \frac{c/a n}{5\pi\beta} T \\ &= \frac{z}{5} \tau_a = e\text{-damping timescale} \end{aligned}$$

so PR drag causes $a, e \rightarrow 0$
among $10 \mu\text{m} < R < 100 \mu\text{m}$ dust.
in $\tau \sim 10^4 \text{ or } 5 \text{ yrs}$

so interplanetary dust quickly drains
into the sun via PR drag.

The fact that the SS is filled w/ dust
tells us the interplanetary dust complex is
replenished by outgassing comets and colliding asteroids

Another calculation using Gauss' Planetary Eqns.

text prob 3.8:

Planets are not perfect spheres; they are oblate due to rotational flattening; they can also have tidal bulges raised by orbiting satellites. The gravitational potential of a rotating gas giant planet can be written

↑
fatter at equator

$$\Phi(r) = -\frac{GM_p}{r} \left[1 - \sum_{n=1}^{\infty} J_n \left(\frac{R_p}{r}\right)^n P_n(\sin\varphi) \right]$$

R_p = planet's mean radius

↑
coefficient, usually smaller for higher n

$P_n(\sin\varphi)$ = Legendre polynomial

φ = latitude above/below planet's equator
 J_n = zonal harmonic for even n .

for gas giants, the J_n where n is odd is usually very small, so for satellites in/near planet's equator at $r \approx R_p$

$$\Phi(r) \approx \Phi_0 + \Phi_2 + \text{negligible terms}$$

$$\Phi_0 = -\frac{GM_p}{r} = \text{Kepler potential}$$

$$\Phi_2 = \frac{GM_p}{r} J_2 \left(\frac{R_p}{r}\right)^2 P_2(\sin\varphi) = -\frac{GM_p J_2 R_p^2}{2r^3}$$

Legendre polynomial $P_2(\sin\varphi) = -\frac{1}{2}$, see A.26

so ϕ_2 = gravitational potential
of the non-spherical part of
the planet's gravity

$$a_r = -\frac{d\phi_2}{dr} = -\frac{3GM_p J_2 R_p^2}{2r^4}$$

= radial acceleration due to
oblate planet's J_2

Saturn is the most oblate planet in
Solar System, has $J_2 = 0.016$

for a close satellite having r just
above R_p so $r = R_p$,

$$|a_r| \approx \frac{3}{2} J_2 \left(\frac{GM_p}{r^2} \right)$$

\Rightarrow gravity due to Saturn's oblate
figure is $\approx 2\%$ of planet's $\frac{GM_p}{r^2}$

Plug a_r into $\dot{\omega} =$ rate at which satellite's longitude of perigee varies, ie its precession rate.

$$\dot{\omega} = \frac{2A_0 \sin f - a \cos f}{e a n}$$

$$a_0 = ?$$

$$\text{so } \dot{\omega} = + \frac{\cos f}{e a n} \frac{3GM_p J_2 R_p^2}{2r^4}$$

from problem 7.11

$$\text{where } \cos f \approx \cos M + e(\cos 2M - 1) + O(e^2)$$

$$r \approx a(1 - e \cos M) + O(ae^2)$$

$$\text{so } \dot{\omega} = \frac{3GM_p J_2 R_p^2 (\cos M + O(e))}{2e a^5 n (1 - e \cos M)^4}$$

$$GM_p = n^2 a^3$$

$$\dot{\omega} = \frac{3n J_2 R_p^2}{2e a^2} \left[\cos M + e(\cos 2M - 1) \right] (1 + 4e \cos M)$$

which again involves many periodic terms, but the sinusoidal contributions to $\dot{\omega}$ sum to zero every orbit

So time average $\dot{\omega}$ to get the secular rate at which ω varies

$$\langle \dot{\omega} \rangle = \frac{3J_2}{2e} \left(\frac{R_p}{a} \right)^2 n \left(\cos i + 4e \cos^2 i + e(\cos 2i - 1) \right) + O(e^2)$$

what is $\langle \cos i \rangle$?

$\langle \cos 2i \rangle$?

so $\langle \cos i \rangle = e$

$$\text{and } \langle \dot{\omega} \rangle = \frac{3}{2} J_2 \left(\frac{R_p}{a} \right)^2 n$$

= rate at which the satellite's
long of peri advances
due to planet's oblateness

